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(54) Title: A METHOD FOR IMPROVING THE HYDROLYTIC RESISTANCE OF ARAMID FIBER

(57) Abstract

A process for improving the hydrolytic resistance of aramid fiber, particularly poly(p-phenylene terephthalamide) fiber is disclosed. The process comprises coating aramid fiber with an aqueous fluoropolymer dispersion and drying the fiber while curing the coating to its surface.

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-1-TITLE

A METHOD FOR IMPROVING THE

HYDROLYTIC RESISTANCE OF ARAMID FIBER

BACKGROUND OF THE INVENTION

Field of the Invention

The present invention provides a process for improving the hydrolytic resistance of aramid fiber by coating such fiber with an aqueous fluoropolymer dispersion. The invention also contemplates poly(p-phenyleneterephthalamide) aramid fiber having improved hydrolytic resistance.

Description of the Prior Art

It is known in the art that coating aramid fiber with fluorocarbon containing material improves certain physical and chemical properties of the fiber.

For example, Trask, United States Patent,
4,232,087 discloses a method of coating "Nomex" aramid
fibers with a dispersion comprised of polytetrafluoroethylene particles in the presence of water and a water
soluble chromium complex of a long chain fluorochemical to
improve the air permeability, acid resistance, water
repellency, and oil repellency of the fibers.

Sasaki et al., United States Patent, 4,337,155 discloses preparing an emulsion of a fluorine-containing polymeric resin and then coating the emulsion onto wholly aromatic polyamide fiber material to improve the air permeability and acid resistance of the material.

Fasick et al., United States Patent, 3,378,609, the disclosure of which is specifically incorporated herein by reference, discloses compositions based upon homopolymers or copolymers derived from the monomer,

 $CH_2=C(CH_3)CO_2CH_2CH_2C_nF_{2n+1}$

wherein n is 3 to 14. The compositions may then be applied as a water dispersion to provide oil and water

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repellent properties to films, fibers, yarns, fabrics, and other articles.

SUMMARY OF THE INVENTION

Despite the development of different fluorocarbon containing coatings for different fibers, there is still a need to provide a suitable coating to improve the hydrolytic resistance of aramid fiber. The present invention relates to treating aramid fiber with a dispersion of fluoropolymer in water, in order to improve the hydrolytic resistance of such fiber. The invention provides a process of uniformly coating aramid fiber with an aqueous dispersion comprising a polymer of ethylenically unsaturated monomers, a major proportion by weight of which is at least one fluorinated alkyl methacrylate polymer of the monomer,

CH2=C(CH3)CO2CH2CH2CnF2n+1

wherein n is 3 to 14. Preferably, the polymer is a copolymer derived from about 75% by weight of the aforementioned fluorinated methacrylate monomer and about 25% by weight of a non-fluorine containing monomer such as 2-ethylhexylmethacrylate. The fiber is then dried while the coating is cured to its surface, preferably by heating the fiber for 15 to 60 minutes at a temperature in the range of 1303 to 1703C.

preferably, poly(p-phenylene terephthalamide) aramid fiber is uniformly coated with a dispersion of fluoropolymer in water such that the amount of fluorocarbon containing coating is in the range of 0.25 to 2% based on total weight of the coated fiber. In a preferred embodiment, the poly(p-phenylene terephthalamide) aramid fiber thus prepared exhibits an improvement in hydrolytic resistance by greater than 20% compared to an uncoated poly(p-phenylene terephthalamide) aramid fiber.

DETAILED DESCRIPTION OF THE INVENTION

The present invention provides a process for improving the hydrolytic resistance of aramid fiber, particularly poly(p-phenylene terephthalamide) aramid fiber. The process includes uniformly coating the aramid fiber with a dispersion of fluoropolymer in water, and then drying the fiber while curing the coating to its surface.

The fluoropolymer dispersions employed in the practice of the invention are disclosed in the aforementioned Fasick et al. U.S. Patent 3,378,609. They are based on the fluorinated methacrylate monomer,

CH2=C(CH3)CO2CH2CH2CnF2n+1
wherein n is 3 to 14. There may be used homopolymers of
the aforementioned fluorinated methacrylate monomer with
one or more other non-fluorine containing monomers.
Copolymers of at least about 50% by weight of the
fluorinated methacrylate monomer with up to about 50% by
weight of one or more copolymerizable non-fluorine
containing monomers may also be used. Various examples of
such copolymerizable monomers and remaining monomers of
the homopolymers are those disclosed in column 4, lines 3
to 57 of Fasick et al.

A preferred fluoropolymer of the invention is a copolymer of about 75% by weight of the fluorinated methacrylate monomer,

CH₂=C(CH₃)CO₂CH₂CH₂C_nF_{2n+1} wherein n varies from 6 to 14 and about 25% by weight of 2-ethylhexylmethacrylate. The fluorinated methacrylate monomer is made by reacting methacrylic acid with a

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mixture of alcohols,

$C_nF_{2n+1}CH_2CH_2OH$,

wherein n is 6 to 14, with an average value of about 8.

If desired, the fluoropolymer dispersion may optionally contain other polymers, such as for example a copolymer containing a small amount of a crosslinking agent.

The fluoropolymer dispersion is then applied to the aramid fiber when the fiber is either wet or dry. conventional coating method for example, immersing or spraying, can be used, but it is important that the dispersion is of a suitable viscosity to be uniformly applied to the fiber. The dispersion can be diluted with water, if needed. A person having ordinary skill in the art will be able to identify which dispersions have suitable viscosities. In a preferred embodiment, wet, never-dried poly(p-phenylene terephthalamide) aramid fiber which is produced according to spinning processes described in Blades, United States Patent, 3,767,756 and Yang, United States Patent, 4,340,559 is immersed in a coating bath containing the fluoropolymer dispersion at room temperature. Preferably, the coating bath is diluted to contain 1% by weight of the preferred fluoropolymer dispersion, a copolymer of about 75% by weight of the fluorinated methacrylate monomer,

 $\label{eq:CH2} \text{CH}_2\text{=C(CH}_3)\text{CO}_2\text{CH}_2\text{C}_n\text{F}_2\text{n}+1 \\$ wherein n varies from 6 to 14, and about 25% by weight of 2-ethylhexylmethacrylate.

After the aramid fiber is uniformly coated with the dispersion, the fiber is dried while the fluorocarbon containing coating is cured to its surface by techniques known in the art. Preferably, curing is performed by heating the fiber for 15 to 60 minutes at a temperature in the range of 1303 to 1703C. Longer heating periods are required with lower temperatures, and vice-versa. At 1503C, for example, a drying time of 30-60 minutes is needed. Preferably, the aramid fiber is uniformly coated with the fluoropolymer dispersion such that the amount of fluorocarbon containing coating is in the range of 0.25 to 2% based on the total weight of the coated fiber. In a preferred embodiment, the cured fluorocarbon containing coating improves the hydrolytic resistance of the aramid fiber by greater than 20% compared to an uncoated fiber.

Testing Procedures

Tensile Properties

Tenacity is reported as breaking strength divided by linear density. Modulus is reported as the slope of the initial stress/strain curve converted to the same units as tenacity. Elongation is the percent increase in length at break. Both tenacity and modulus are first computed in g/denier units which, when multiplied by 0.8838, yield dN/tex units. Each reported measurement is the average of 5 breaks.

Tensile properties for yarns are measured at 243C and 55% relative humidity after conditioning under test conditions for a minimum of 14 hours. Before testing, each yarn is twisted to a 1.1 twist multiplier (for example, nominal 1500 denier yarn is twisted about 0.8 turns/cm). Each twisted specimen has a test length of 25.4 cm and is elongated 50% per minute (based on the original unstretched length) using a typical recording stress/strain device.

The twist multiplier (TM) of yarn is defined as:

TM=
$$\frac{\text{tpi V Denier}}{73} = \frac{\text{tpc V dtex}}{30.3}$$

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Wherein tpi= turns per inch and tpc= turns per centimeter.

In the following examples, parts and percentages are by weight unless otherwise indicated.

COMPARATIVE EXAMPLE

A finish-free wet, never-dried poly(p-phenylene terephthalamide) aramid yarn was produced according to spinning processes described in Blades, United States Patent, 3,767,756 and Yang, United States Patent, 4,340,559. The aramid fiber was then tested for its hydrolytic resistance. As shown in Table I, the test yarn had a linear density of 1462 denier at 1.5 dpf (denier per filament). It gave tensile properties of 21.4 gpd (grams per denier) tenacity, 3.5% elongation at break, and 542 gpd initial modulus. A 5 m long skein of the yarn was tested for hydrolytic resistance by immersing the yarn in a 10% NaOH solution at 953C for 20 hours. The test yarn skein was then thoroughly washed with water at room temperature and left to dry in air at zero tension. The hydrolyzed yarn gave a retained tenacity of 4.2 gpd, which was a 19.6% retention of its original tenacity. When the alkaline hydrolysis was extended to 100 hours, the hydrolyzed yarn was too weak to be tested for its tensile properties.

EXAMPLE I

This example illustrates the improved hydrolytic resistance of poly(p-phenylene terephthalamide) aramid yarn after such yarn is coated with a dispersion of fluoro-polymer in water.

The fluoropolymer dispersion is formed as an aqueous dispersion in water of two components, A and B. Component A is a polymer formed by the polymerization of 25% 2-ethylhexylmethacrylate with 75% of the fluorinated

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methacrylate monomer,

CH₂=C(CH₃)CO₂CH₂CH₂C_nF_{2n+1} wherein n varies from 6 to 14 with an average of 8, together with about 0.25% each of N-methylolacrylamide and 2-hydroxyethylmethacrylate. Component B is a terpolymer of100 parts 2-ethylhexylmethacrylate with 2 parts N-methylolacrylamide and 0.5 parts ethylene dimethacrylate. About 8 parts of A is used with about 6 parts of B to produce an emulsion having 14% solids. The fluoropolymer dispersion was added to a coating bath which was then diluted with water until the bath contained 1% of said fluoropolymer dispersion.

A 5 m long skein of the finish-free yarn used as a COMPARATIVE EXAMPLE was then immersed in the bath containing 1% fluoropolymer dispersion at room temperature for 40 hours. The yarn was uniformly coated with the fluoropolymer dispersion such that the amount of fluorocarbon containing coating was about 0.75% of the cured fiber. The yarn was then dried while the coating was cured to its surface at 1503C at zero tension for half an hour. As Table I shows, the coated yarn was subjected to hydrolysis in a 10% NaOH solution at 953C for 20 hours. The hydrolyzed yarn gave a retained tenacity of 15.2 gpd which was a 71.0% retention of its original tenacity. When the hydrolysis was extended to 100 hours, the hydrolyzed yarn gave a retained tenacity of 7.9 gpd which was a 36.9% retention of its original tenacity.

EXAMPLE II

This example illustrates similar improvements in the hydrolytic resistance of poly(p-phenylene terephthalamide) aramid yarn when the yarn is coated with a dispersion of fluoropolymer in water. As shown in Table I, the process of EXAMPLE I was carried out except that

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the time of immersing the yarn in the coating bath containing 1% of the fluoropolymer dispersion was decreased to 1 minute. The yarn was uniformly coated with the fluoropolymer dispersion such that the amount of fluorocarbon containing coating was about 0.6% of the coated fiber. The coated yarn was subjected to hydrolysis in a 10% NaOH solution at 953C for 20 hours. The hydrolyzed yarn gave a retained tenacity of 14.7 gpd which was a 68.7% retention of its original tenacity. When the hydrolysis was extended to 100 hours, the hydrolyzed yarn gave a retained tenacity of 6.8 gpd which was a 31.8% retention of its original tenacity.

TABLE I

EXAMPLE	COMPARAT:	IVE I	II
		•	
Base Yarn	poly(p	-phenylene terep	hthalamide)
Coating Agent	None	1% "Zepel" B	l% "Zepel" B
Immersion Time		40 hours	l min.
	•	•	
AS SPUN YARN			
Yarn denier	1462	1462	1462
Dpf	1.5	1.5	1.5
Tenacity	21.4	21.4	21.4
Elongation, %	3.5	3.5	3.5
Modulus, gpd	542	542	542
HYDROLYZED YARN			
10% NaOH/953C/20 hours	5		•
Retained tenacity,			
gpđ	4.2	15.2	14.7
% Tenacity retention	19.6	71.0	68.7
HYDROLYZED YARN	•		
10% NaOH/953C/100 hou	rs		
Retained tenacity,			
gpd	~0	7.9	6.8
% Tenacity retention	~0	36.9	31.8

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CLAIMS:

- 1. A process for improving the hydrolytic resistance of aramid fiber by the steps of:
- a) coating aramid fiber with an aqueous fluoropolymer dispersion to obtain a uniform fluorocarbon
 containing coating on the fiber, said aqueous fluoropolymer dispersion comprising a polymer of ethylenically
 unsaturated monomers, a major proportion by weight of
 which is at least one fluorinated methacrylate monomer of
 the structure,

CH2=C(CH3)CO2CH2CH2CnF2n+1

wherein n has a value of from 3 to 14;

- b) drying the fiber while curing said coating to its surface.
- 2. A process in accordance with claim 1 wherein said polymer is a copolymer of the fluorinated methacrylate monomer with 2-ethylhexylmethacrylate.
- 3. A process in accordance with claim 1 wherein the curing of the fluorocarbon containing coating to the surface of the fiber is effected by heating the fiber for 15 to 60 minutes at a temperature in the range of 1303 to 1703C.
- 4. A process in accordance with claim 1 wherein the aramid fiber is poly(p-phenylene terephthalamide).
- 5. A poly(p-phenylene terephthalamide) aramid fiber having improved hydrolytic resistance produced in accordance with claim 4 wherein the amount of fluorocarbon containing coating is in the range of 0.25 to 2% based on total weight percent of the coated fiber.
- 6. A poly(p-phenylene terephthalamide) aramid fiber having improved hydrolytic resistance in accordance with claim 5 wherein said fiber exhibits hydrolytic resistance by greater than 20%.

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International Application No

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